

Mitigating Stress Corrosion Cracking and Irradiation Damage of Austenitic Alloys by Laser Shock Peening

Fei Wang¹, Xueliang Yan¹, Xiaoxing Qiu¹, Chenfei Zhang², Yongfeng Lu², Qing Su³, Michael Nastasi³, Bai Cui¹

¹Department of Mechanical & Materials Engineering, University of Nebraska–Lincoln., ²Department of Electrical Engineering, University of Nebraska–Lincoln, ³Nebraska Center for Energy Sciences Research, University of Nebraska–Lincoln

Background

Due to the increasing demand for energy and environmental concerns related to emissions from fossil fuels, DOE launched the “Generation-IV Initiative” in 2000 to further advance nuclear energy systems design. In Generation-IV reactors, structural materials need to endure much higher neutron doses (>300 dpa), higher operation temperatures (> 200 °C over an 80 year lifetime), and extremely corrosive coolants (such as supercritical water, gas, sodium, or Pb).

Oxide-dispersion-strengthened (ODS) alloys are promising candidate structure materials for Generation-IV reactors. In their microstructure, dispersions of Y-Ti-O nanoparticles (< 10 nm) in the stainless steel matrix (Figure 1) result in superior resistance to creep and irradiation damage at elevated temperatures. However, ODS **austenitic** alloys, such as ODS 304, 310 and 316 stainless steels, are susceptible to intergranular stress corrosion cracking (SCC) in primary and supercritical water environments. SCC is the growth of cracks due to the simultaneous action of a tensile stress and a corrosive environment. Material degradation due to SCC costs the U.S. nuclear industry over \$10 billion in the last 30 years.

The goal of this research is to improve the SCC and irradiation damage resistances of ODS **austenitic** alloys using laser shock peening (LSP).

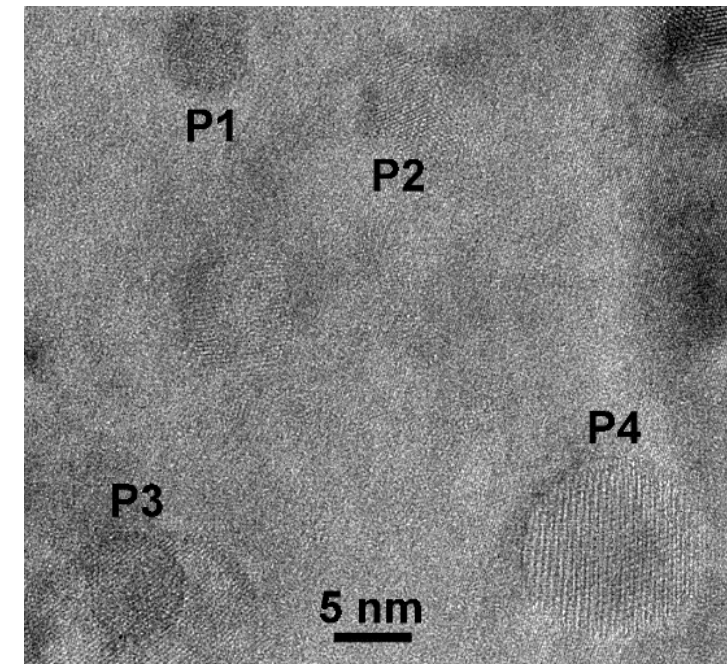
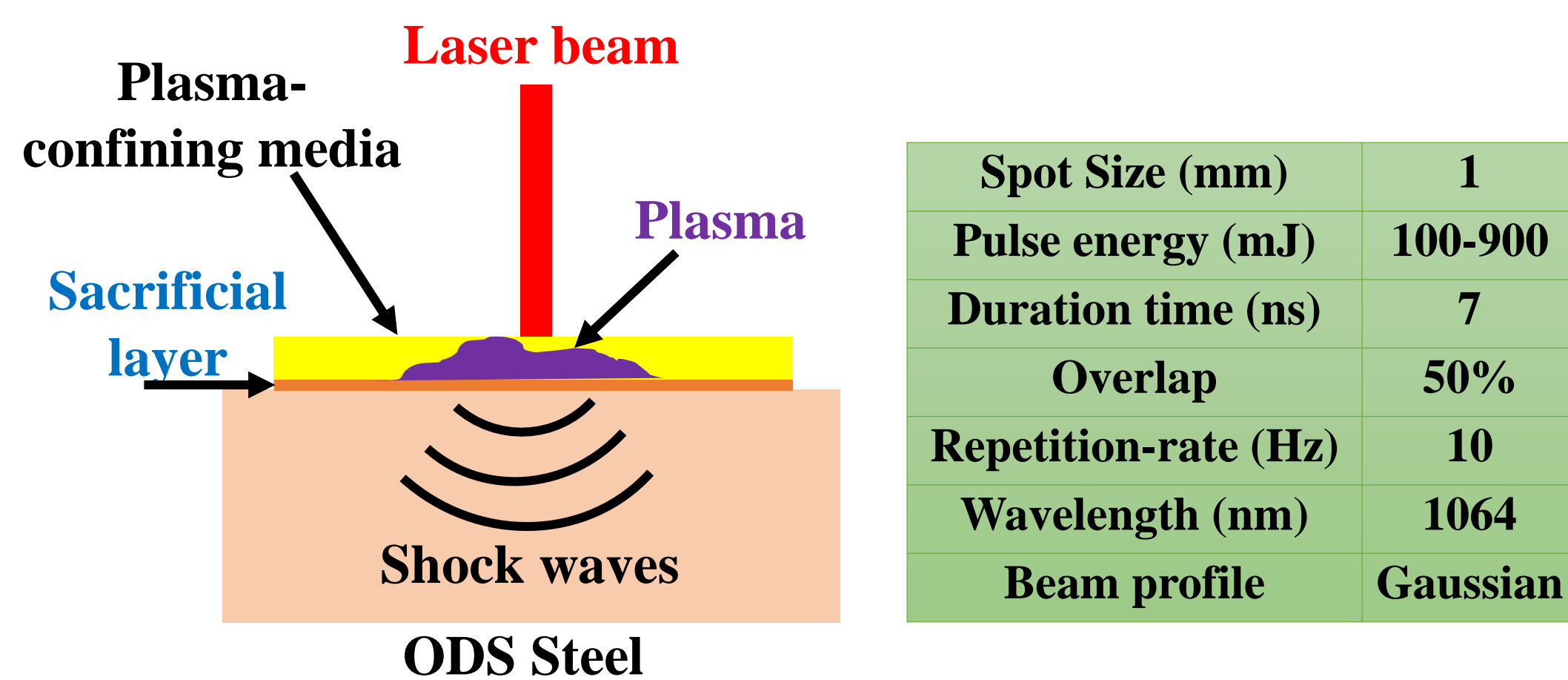


Figure 1. High-resolution TEM image of the ODS 310 austenitic stainless steel used in this project. Y-Ti-O nanoparticles (“P”) are labeled.

Experiment

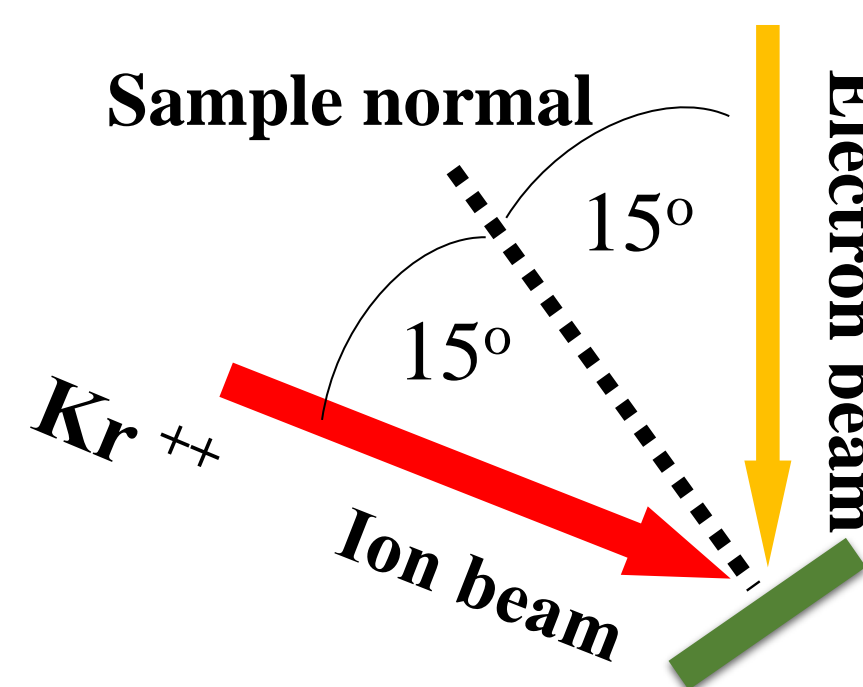
• Laser shock peening

In the LSP process, the rapid expansion of a plasma on the surface generates shock waves into the bulk material, which induce significant compressive residual stresses (0.1-1 GPa). LSP is superior to the mechanical shot peening in the benefits of deeper penetration of compressive stress, shorter process, precise control, accuracy, flexibility and no contamination.



• In situ irradiation

Figure 2. The IVEM-Tandem in-situ irradiation facility



• Stress corrosion cracking

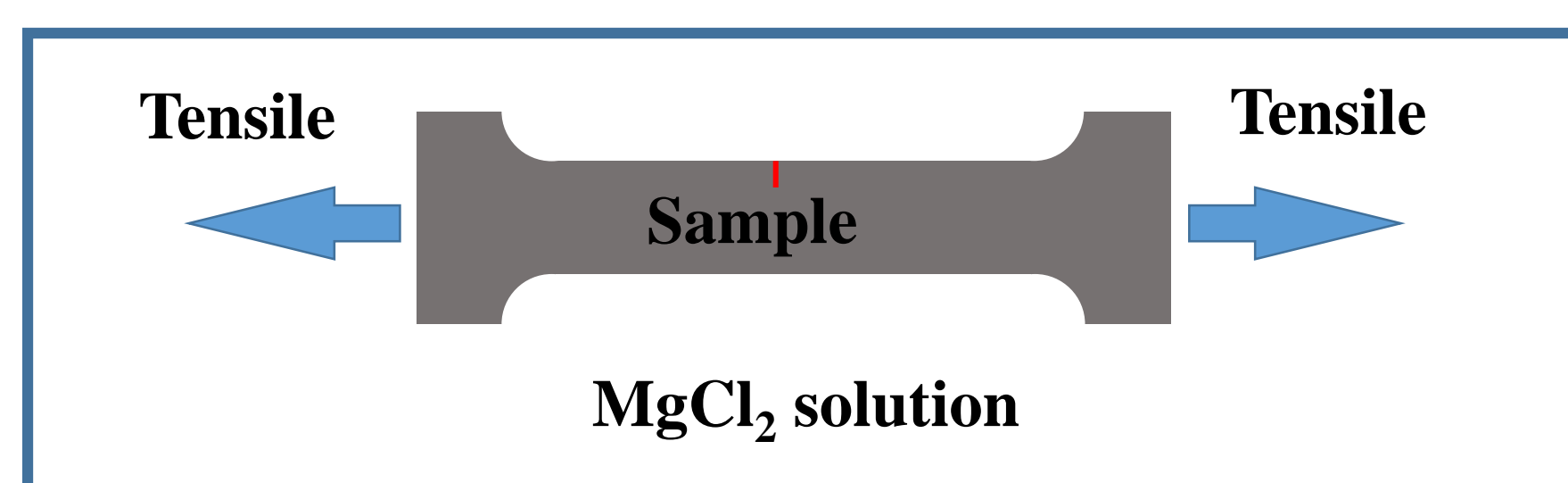


Figure 3. Schematic view of SCC set up.

Prevention of SCC by LSP

LSP is a new approach that can prevent SCC of **austenitic** stainless steels, but the mechanisms are poorly understood. Preliminary test data shows that:

- (1) ODS **austenitic** alloys are susceptible to SCC. The crack growth rate in the ODS 304 stainless steel is slightly higher than the regular 304 steel (Figure 4).
- (2) SCC occurred significantly in the original 304 stainless steel sample, which shows transgranular cracks (Figure 5a). In contrast, no apparent cracks are present in LSP-treated samples under the test environment (Figure 5b).

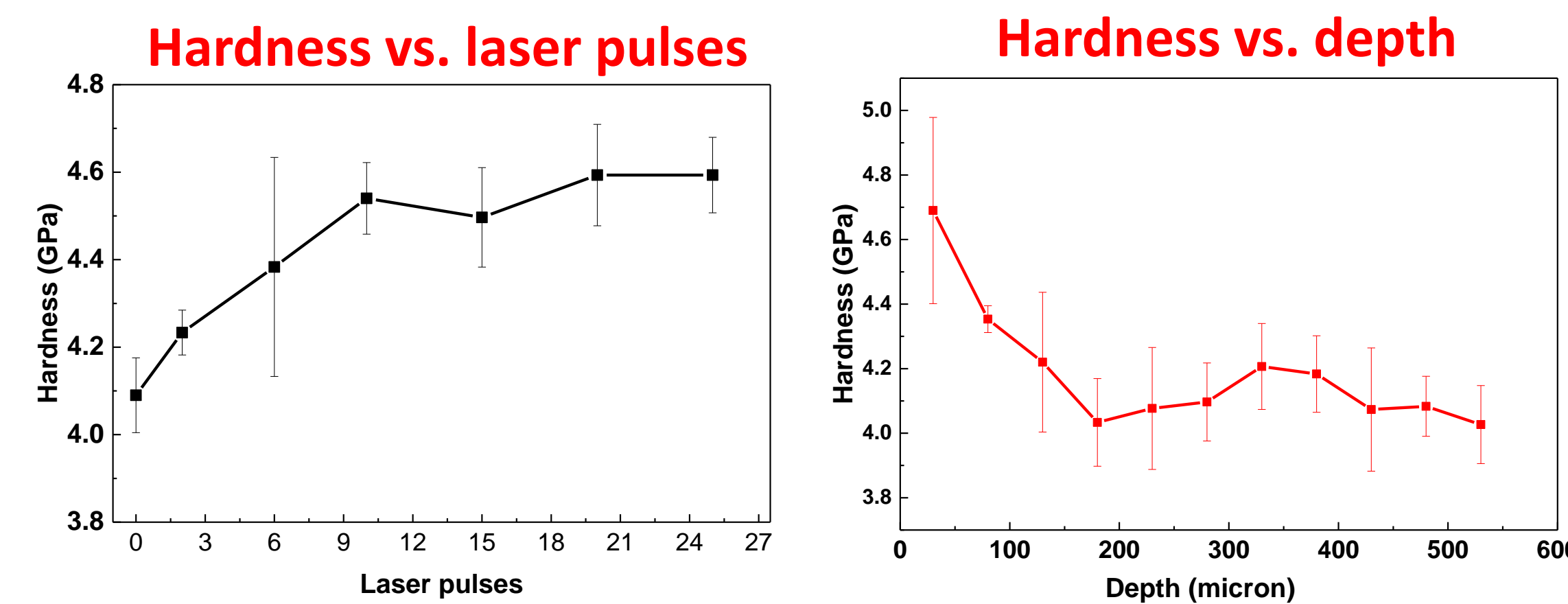


Figure 4. The hardness change of sample after laser peening: (a) hardness vs time; (b) hardness distribution along depth.

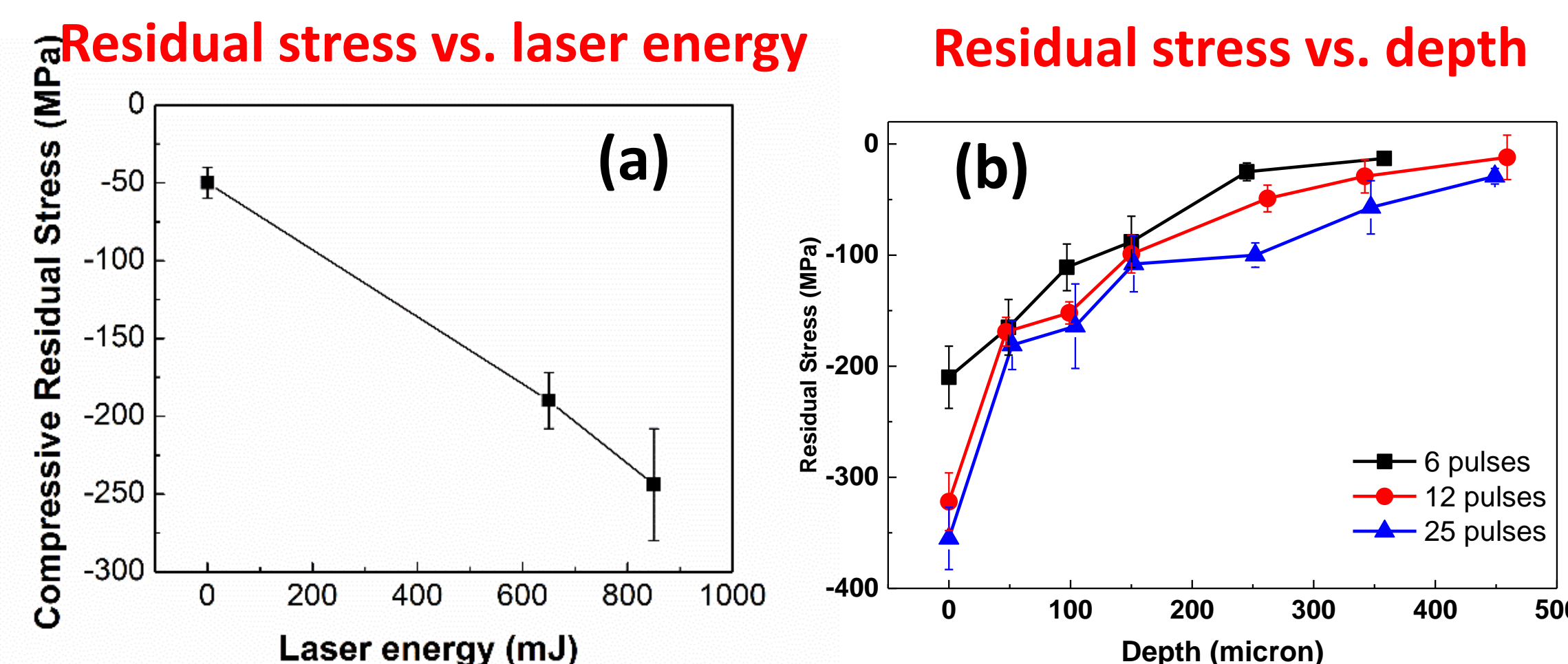


Figure 5. (a) The surface residual stress of sample after laser peening. (b) residual stress distribution along depth.

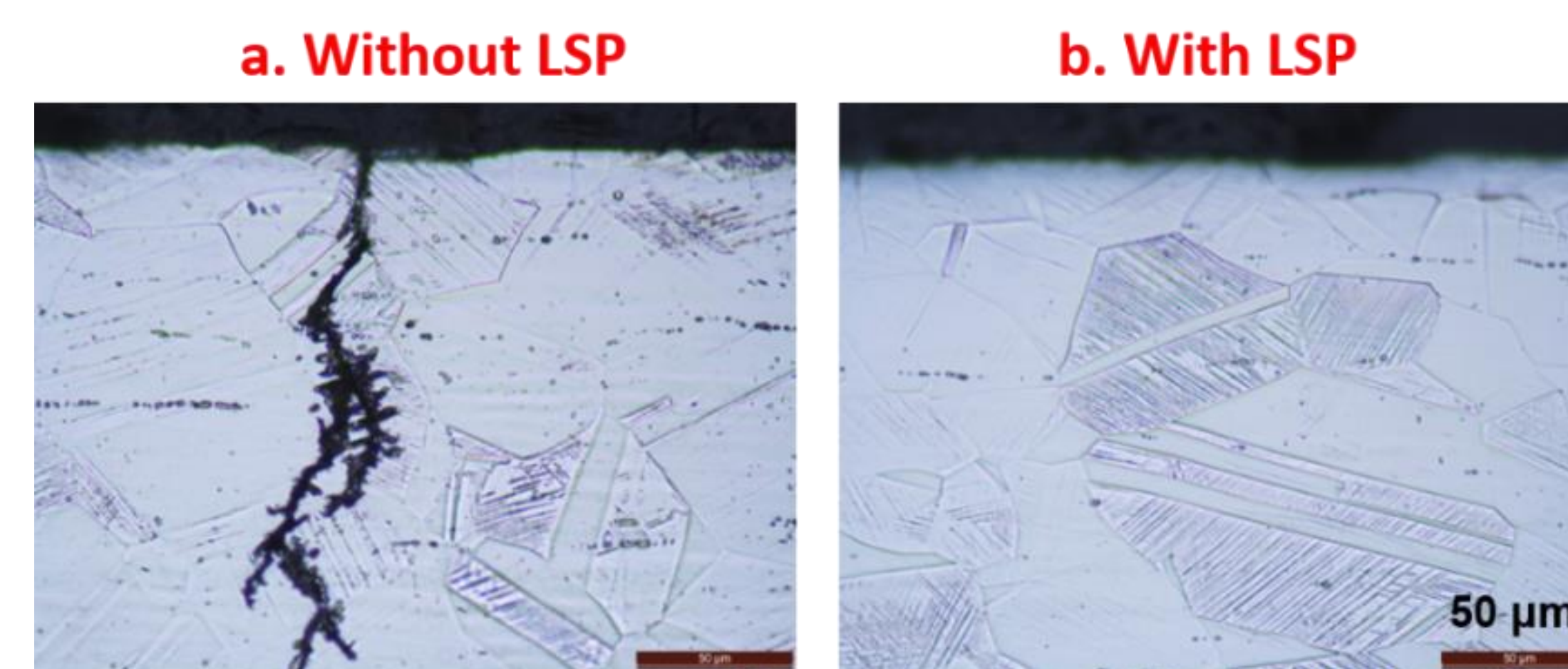


Figure 6. Stress corrosion cracking (SCC) test results in a hot water environment with 42% MgCl₂ at 144 °C for 168 hours: (a) original 304 stainless steel; (b) 304 stainless steel treated by LSP with 850 mJ laser pulse energy and 4 laser pulses. The images are optical micrographs of the cross-section microstructure.

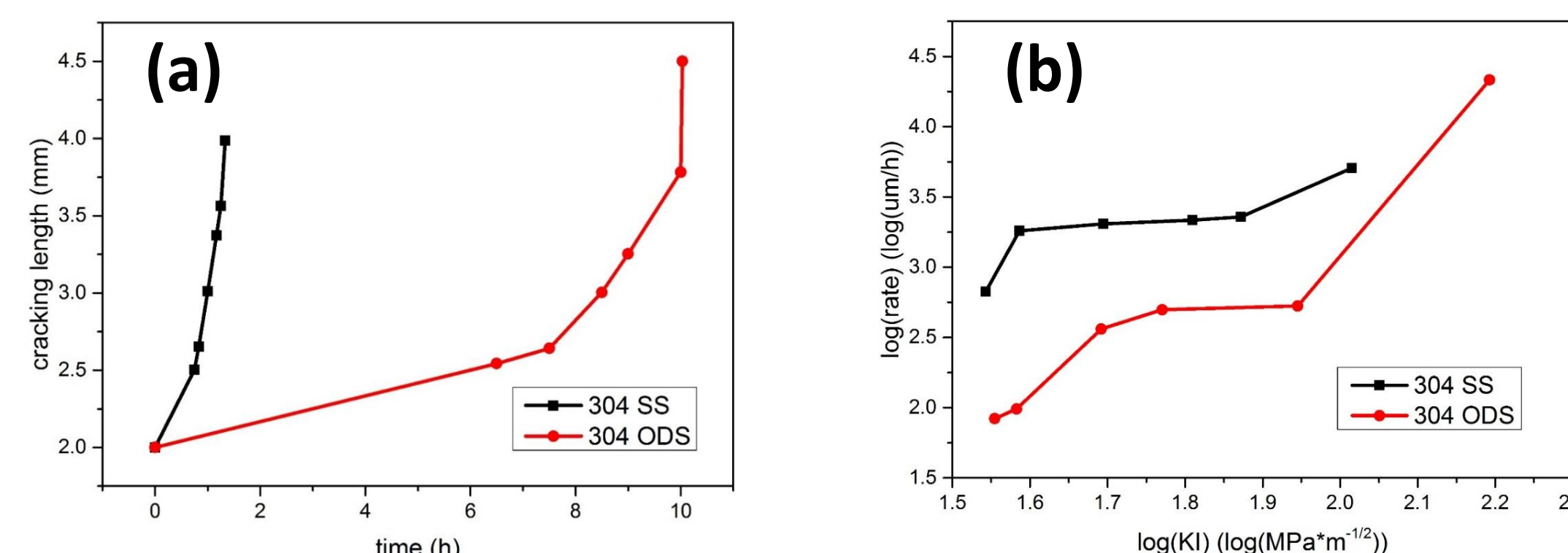


Figure 7. The SCC behavior of 304 stainless steel and 304 ODS: (a) crack length vs time; (b) crack rate vs stress intensity factor K_I .

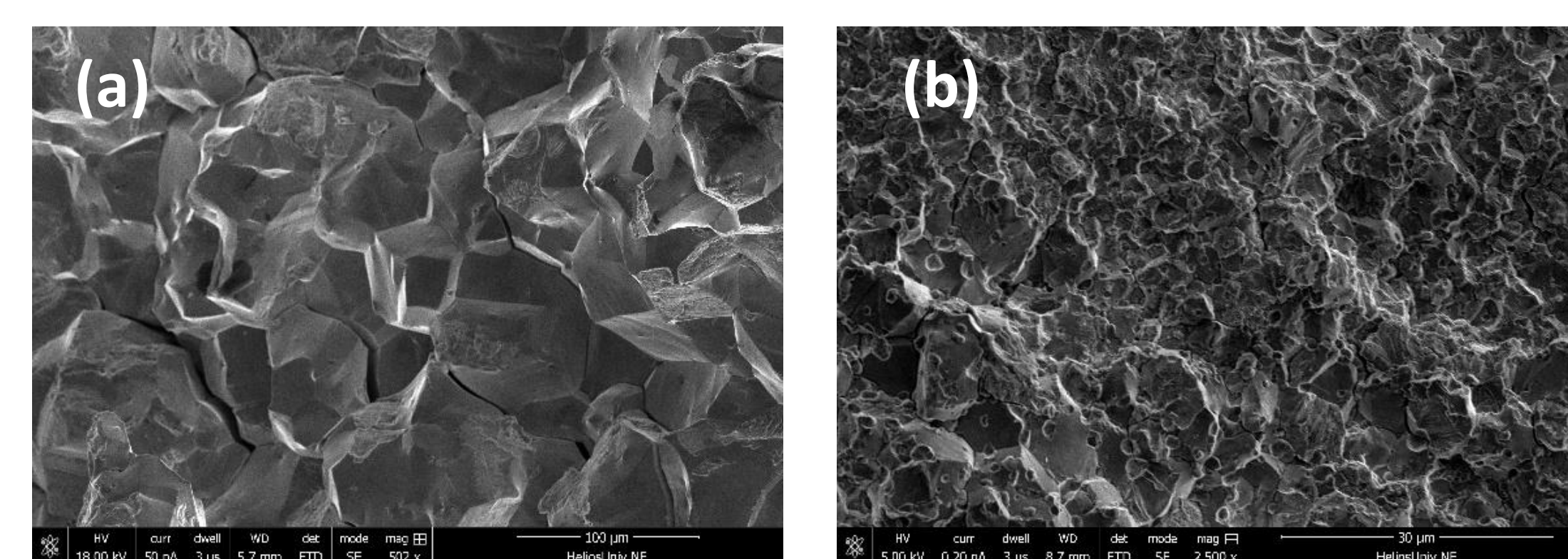


Figure 8. Fracture surface of (a) 304 stainless steel and (b) 304 ODS alloy.

Microstructures of Laser-Peened Stainless Steels

Interaction of laser-driven shock waves with **austenitic** stainless steels results in dislocation networks, stacking faults, and deformation twins in the near surface, suggest that significant plastic deformation occurred in stainless steels during the LSP process. When the pressure of shock waves exceed the yield strength of an alloy, it will experience an extremely high strain-rate (10^6 – 10^8 s⁻¹) during a short period of time and be dynamically yielded.

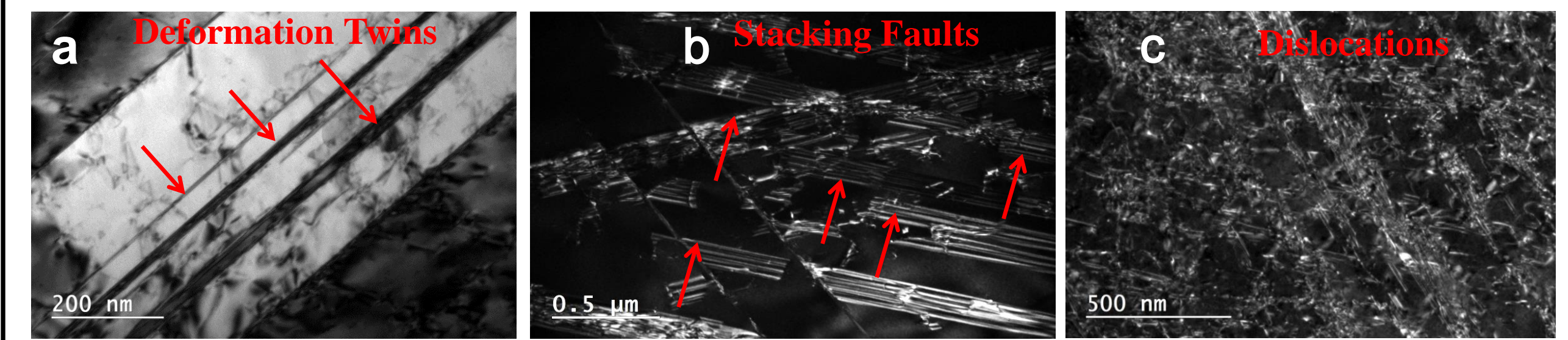


Figure 9. Typical transmission electron microscopy (TEM) images of near-surface microstructures of 304 **austenitic** stainless steel treated by laser shock peening (LSP): (a) deformation twins (arrowed); (b) stacking faults (arrowed); (c) high-density dislocations.

During *in situ* TEM irradiation experiments observed that twin boundaries and dislocations in laser-peened 304 steels can serve as effective sinks for the annihilation of irradiation defects. As a result, the irradiation defect density in laser-peened 304 steels is just 15~25% of that in untreated samples.

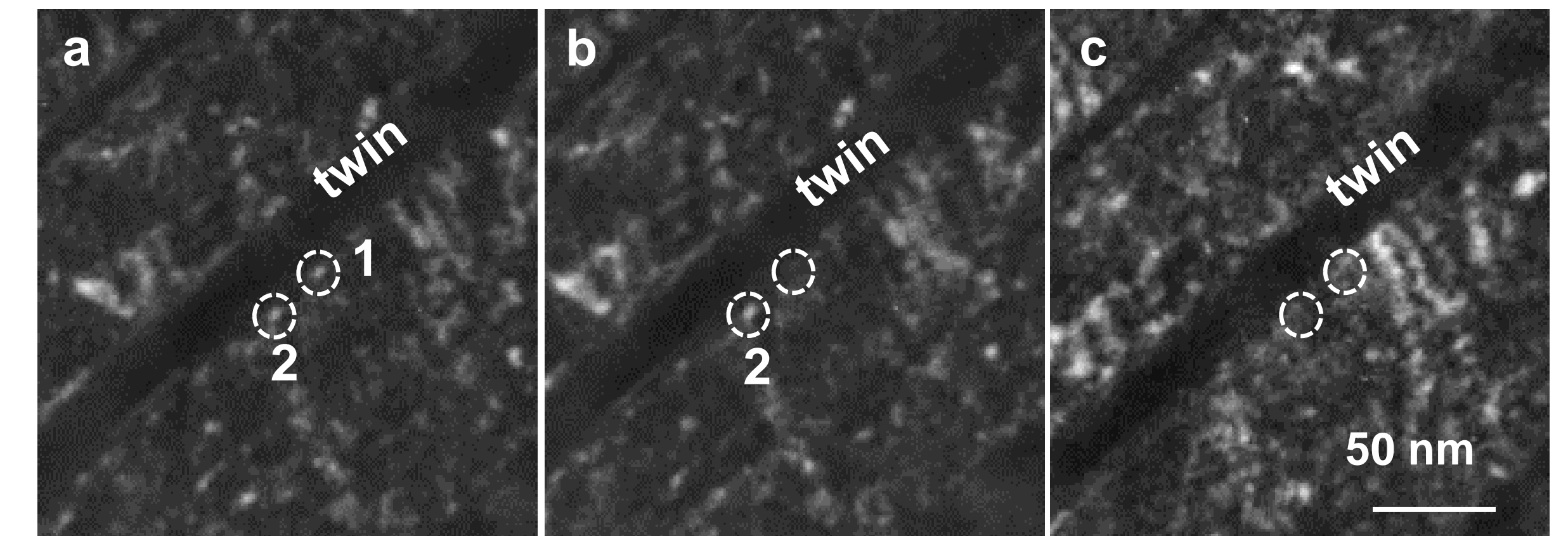


Figure 10. Annihilation of irradiation defects by a twin boundary in laser-peened 304 steel sample: (a) two defect clusters 1 and 2 (bright spots in circles) formed at 0s; (b) defect cluster 1 was annihilated at 4s; (c) defect cluster 2 was annihilated at 32s.

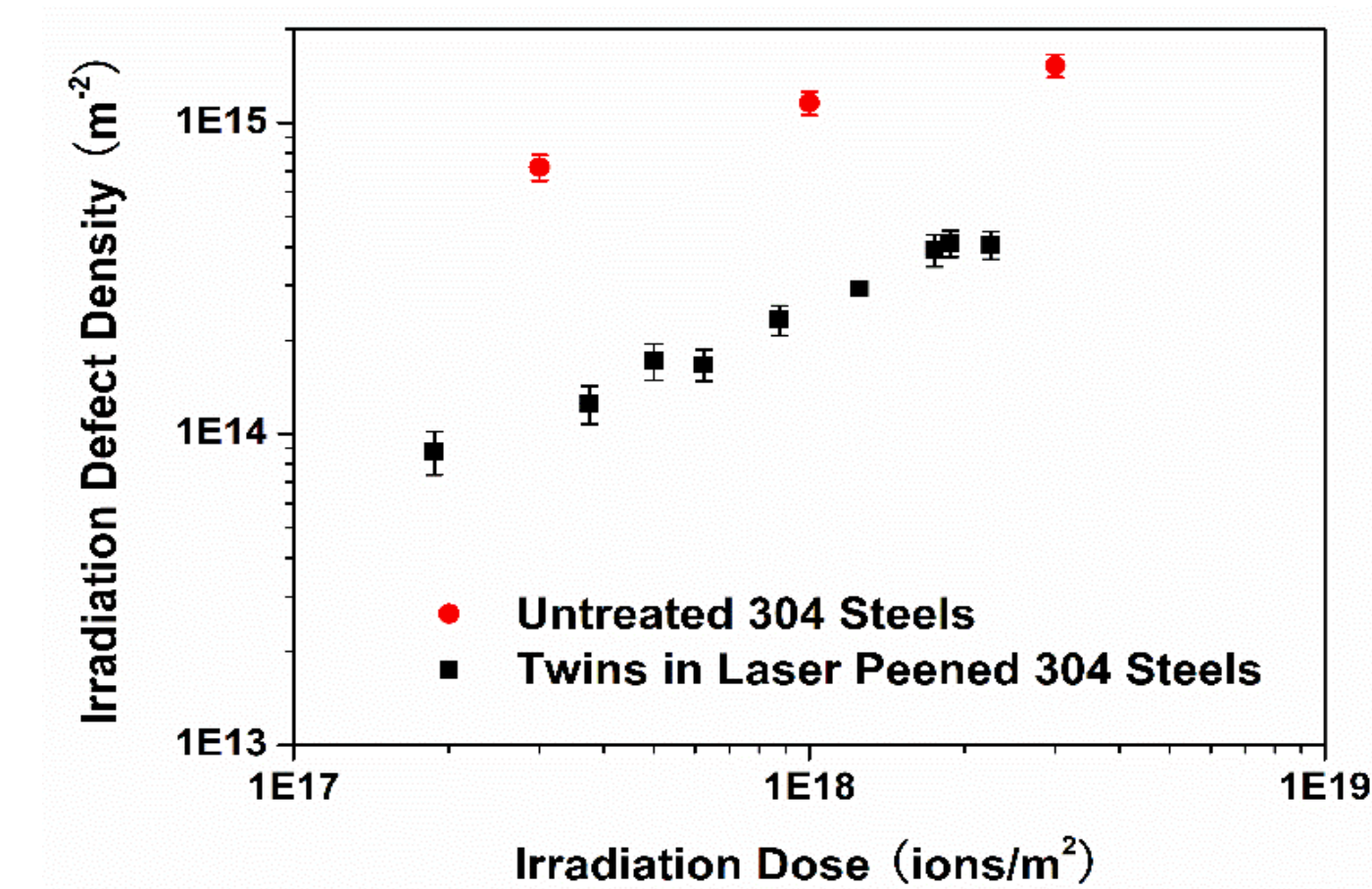


Figure 11. Evolution of irradiation defect density in untreated and laser-peened 304 steels (twin region) under 1 MeV Kr⁺ irradiation at room temperature

Conclusions

- The LSP process has been used to prevent SCC and reduce the irradiation damage of ODS austenitic alloys in high-temperature water environment.
- These effects are related to a deep penetration of compressive residual stress, and the microstructural changes in the near surface by the interaction of laser-driven shock waves with the materials.
- The laser-driven shock waves in the LSP process can produce severe plastic deformation in austenitic stainless steels. Dislocation networks, stacking faults, and deformation twins were generated in the near-surface region of laser-peened 304 stainless steels.
- The dislocation network and incoherent twin boundaries can serve as high strength sinks for the annihilation of irradiation defects clusters during the heavy ion irradiation.

Acknowledgement

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